Comparative Valuation of Precise and Approximate Non-Linear Models of an AC Discrete Voltage Regulator and Vector Analysis of Its Parameters

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ABSTRACT

The paper presents a review on the problems of the analysis of autotransformer discrete alternating voltage regulators. Most often the discrete regulation of AC voltages is achieved by power electronic converters based on a transformer (autotransformer) and switching by the means of controllable semiconductor switches.

The present work is dedicated to the comparison between precise and approximate non-linear models of autotransformer discrete alternating voltage regulator with changing input voltage and commutation angle of the semiconductor switches and to the vector measurements in an autotransformer discrete voltage regulator.

Keywords: AC voltage regulator, semiconductor switch, thyristor, vector analysis, vector measurements.

1 INTRODUCTION

In Fig.1 the equivalent circuit of an autotransformer discrete AC voltage regulator (ADACVR) with four terminals and four controllable semiconductor switches (CSS) is shown. The equivalent circuit corresponds to the precise model where the circuit includes the parameters of the magnetic circuit, the commutation groups, the switch-off assemblies, the parameters of the separate sections of the winding and it takes into account the existing non-linearities. In the approximate non-linear model the losses in the autotransformer core are not considered, the semiconductor switches are accepted for ideal and the RC groups, which shunt the thyristors in the semiconductor switches, are not taken into account [1]. The adopted control algorithm is connected with switching at random moment as the commutation is always performed between two neighbouring semiconductor switches [2, 3].

The feeding with control pulses is suspended to the thyristor switch, which will be turned off (the switch remains conductive until the natural commutation of the thyristors inside it), and the other switch starts to be fed with control pulses. The equivalent circuits of the precise and approximate non-linear models and their mathematical descriptions are presented in details in literature [4, 5].

The aim of the current work is the comparative research into the loading (the semiconductor switches, the autotransformer windings) by vector analysis and vector measurements of the quantities during the commutation process at different character of the load – R, RL and RC and different commutation angles.

2 ANALYSIS

In this paper a vector analysis at low values of the input voltage of ADACVR is conducted. In this case, the switch K_4 is turned off and the switch K_3 is switched on (Fig.1).

Fig.1. Equivalent circuit corresponding to the precise model of an ADACVR with four CSS ($K_1 \div K_4$) at input voltage change.

At the same time, at certain angles φ of the commutation process, it is possible r_4 and L_4 (Fig.1) to be connected in short circuit through two thyristors, one from the switch K_4 and one from the switch K_3 respectively, for the time until the natural commutation of the switch K_4 occurs. This mode assumes an overload regime of the fourth section of the autotransformer and the two connected in series thyristors from the switches K_4 and K_3 , when they are triggered.

a) Oscillogram of the input current $i_1(t)$ at $\varphi=270^\circ$.

b) Oscillogram of the output current $i_2(t)$ at $\varphi=270^\circ$.

c) Oscillogram of the current through switch K_3 - $i_3(t)$ at $\varphi=270^\circ$.

d) Oscillogram of the current through switch K_4 - $i_4(t)$ at $\varphi=270^\circ$.

Fig.2. Experimental oscillograms of the currents of the ADACVR for R load and commutation angle $\varphi=270^\circ$.

a) Simulation of the input current $i_1(t)$ at $\varphi=270^\circ$.

b) Simulation of the output current $i_2(t)$ at $\varphi=270^\circ$.

c) Simulation of the current through switch K_3 - $i_3(t)$ at $\varphi=270^\circ$.

d) Simulation of the current through switch K_4 - $i_4(t)$ at $\varphi=270^\circ$.

Fig.3. Computer simulation of the currents of the ADACVR for R load and commutation angle $\varphi=270^\circ$.

a) Oscillogram of the input current $i_1(t)$ at $\varphi=225^\circ$

b) Oscillogram of the current through switch $K_3 - i_3(t)$ at $\varphi=225^\circ$.

Fig.4. Experimental oscillograms of the currents of the ADACVR for RL load and commutation angle $\varphi=225^\circ$.

a) Oscillogram of the input current $i_1(t)$ at $\varphi=225^\circ$.

b) Oscillogram of the current through switch $K_3 - i_3(t)$ at $\varphi=225^\circ$.

Fig.6. Experimental oscillograms of the currents of the ADACVR for RC load and commutation angle $\varphi=225^0$.

a) Simulation of the input current $i_1(t)$ at $\varphi=225^0$.

b) Simulation of the current through switch K_3 - $i_3(t)$ at $\varphi=225^0$.

Fig.5. Computer simulation of the currents of the ADACVR for RL load and commutation angle $\varphi=225^0$.

a) Simulation of the input current $i_1(t)$ at $\varphi=225^0$.

b) Simulation of the current through switch K_3 - $i_3(t)$ at $\varphi=225^0$

Fig.7. Computer simulation of the currents of the ADACVR for RC load and commutation angle $\varphi=225^\circ$.

In case of an active load (R-load) and commutation angle $\varphi=270^\circ$, the results from the experimental oscillograms and the computer simulations with the programme AVTO (developed by the authors) in MATLAB integrated environment, are presented in Fig.2 and Fig.3. In cases of RL and RC loads, the development of the commutation process can be followed in Fig.4 and Fig.5, Fig.6 and Fig.7, respectively. The experimental oscillograms and simulations are taken at commutation angle $\varphi=225^\circ$.

The received experimental data for a concrete regime (closed switch K_4 and opened switch K_3) are shown in Table 1. The analytical data in the table are very close to those from the analysis of the precise model [6, 7, 8, 9, 10]. The numerical values from the simulations with the approximate model of the voltage regulator differ with average deviation 1% (minimum deviation 0,09% and maximum deviation 3%) from those, received by a simulation with the precise model.

Table 1

Type of load	Experimental data			Computer simulations		
	I_1	I_2	U_2	I_1	I_2	U_2
	A	A	V	A	A	V
R	8,45	6,16	219	8,3965	6,1205	218,6
RL	9,75	7,03	219,9	8,5181	6,2016	217,8
RC	2,85	2,15	220,3	2,8034	2,1421	222,6

- *Note:* The loads for the experiments and the simulations, shown in the table, are as follows:

R load - 35,7 Ω ;

RL load - R-35,7 Ω , L-1,76H (connected in parallel);

RC load - R-61,78 Ω , C-38,09 μ F (connected in series).

In Table 2 the vector quantities of the currents and the voltages of the autotransformer discrete regulator from the equivalent circuit in Fig.1 are presented.

Table 2

Type of load	Results from vector measurements of ADACVR		
	$\dot{I}_1$	$\dot{I}_2$	$\dot{U}_2$
	A	A	V
R	$8,45e^{-j0,08}$	$6,16e^{-j0,06}$	219
RL	$9,75e^{-j0,14}$	$7,03e^{-j0,12}$	$219,9e^{j0,06}$
RC	$2,85e^{j0,89}$	$2,15e^{j0,92}$	$219e^{-j0,01}$

3 CONCLUSION

A programme AVTO in MATLAB integrated environment is developed, and it allows visualization of the computer simulations as well as examination of the discrete AC voltage regulator with different loads and parameters of the commutation processes.

A vector analysis and vector measurements of the quantities, referred to the commutation and the regimes in a power semiconductor converter with discrete regulation of the input AC voltage magnitude to the joined consumers have been conducted. A precise and approximate (with certain simplifications) models have been examined at different angles for the commutation process and for different loads.

An approximate non-linear model can be used for a quick engineering calculation of an autotransformer discrete AC voltage regulator with different number of terminals.

Both results – from the experiments and from the computer simulations, show a very good match of the obtained results.

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